

Influence of Inverters Based Sources on Protections Devices

B5 PROTECTION AND AUTOMATION

PS1 - Addressing protection related challenges in network
with low-inertia and low fault-current levels, Q1.02

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Presentation Time to be
Proposed: 3 or 4 min

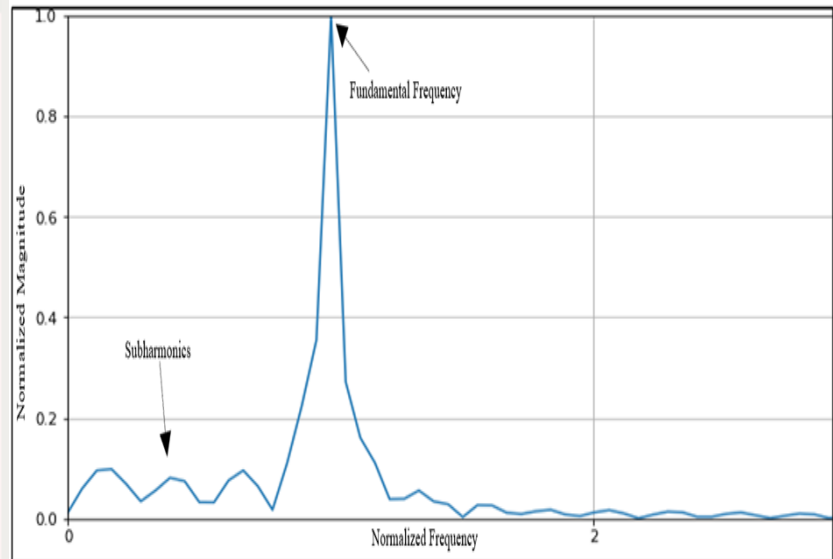
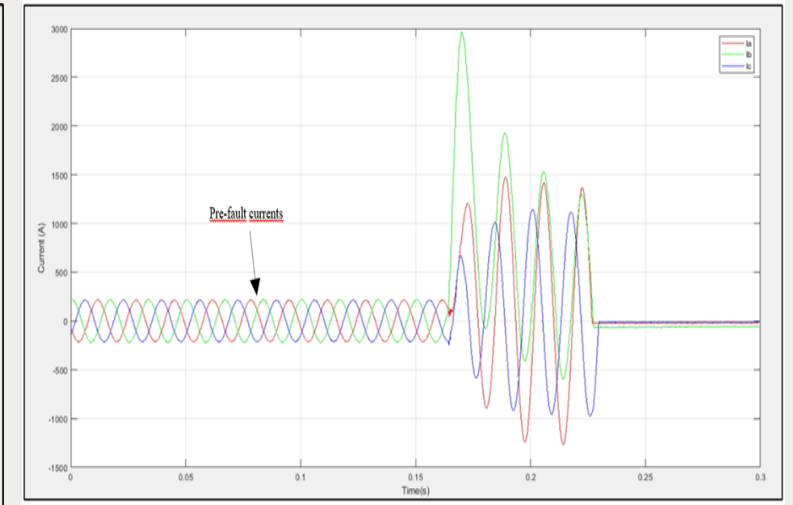
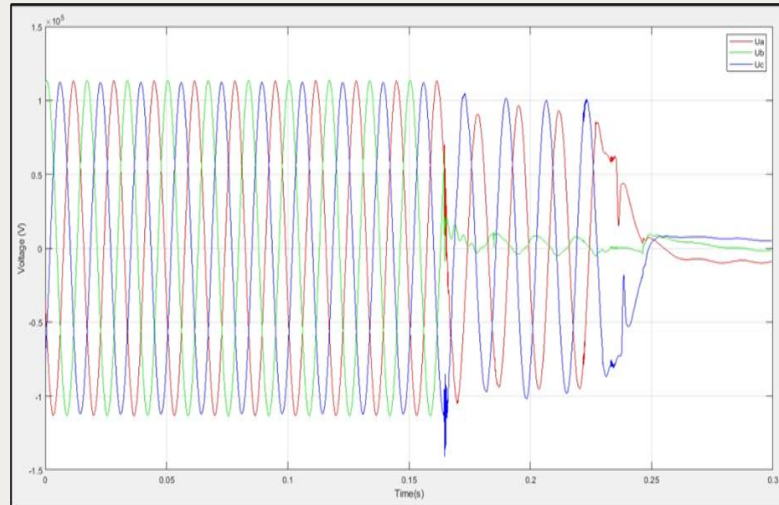
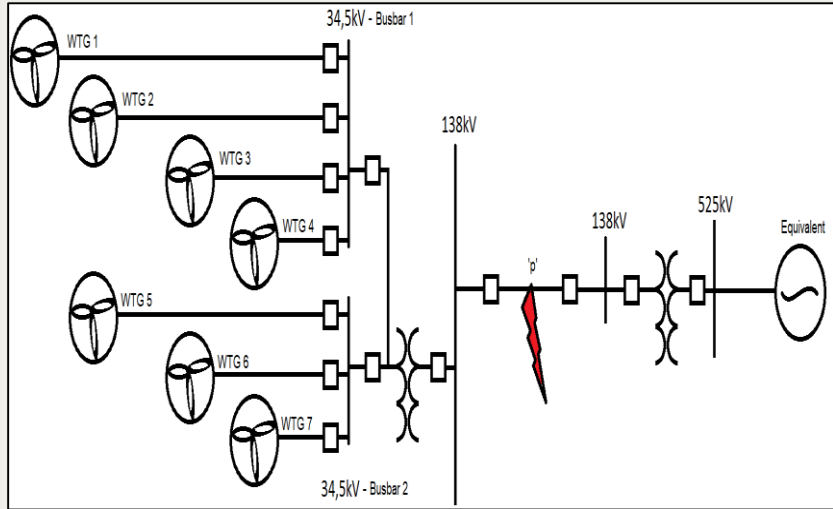
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Question 1.02: Are risks of distance protection maloperation or failure to trip limited to transmission lines directly connected to the wind power plant or do you see broader implications for protection further away from the wind power plant point of connection to the transmission grid?

The main points can be highlighted, in general, as:

- During the **period of the fault** the Inverter Based Source (IBS) waveform output **tends to be distorted** and can **influence** the **expected behaviour** of the **frequency/angle** on the phasor's estimation process;
- IBS **output frequency** could be **unstable** and generate abnormal frequency with **unexpected** Rate-of-Change of-Frequency (**ROCOF**);
- IBS **fault current magnitude contribution** will be **almost nominal value** as limited by the **thermal rating** of the power electronic components;
- IBS **reacts** to a **system fault** with two distinctive period, the **transient** and **steady-state** period. The transient period varies between **half a cycle to 1.5 cycles**;
- IBS fault **current sequence components**, magnitude and angle, will depend on the IBS **control setting** and the generating conditions **before the fault**;
- IBS **control system** tends to contribute with **balance fault currents** during **balanced** and **unbalanced** fault and might not provide **adequate negative sequence components** to be used by the protection and control elements that depends on the negative sequence quantities (it depending on the **grid code requirements**).

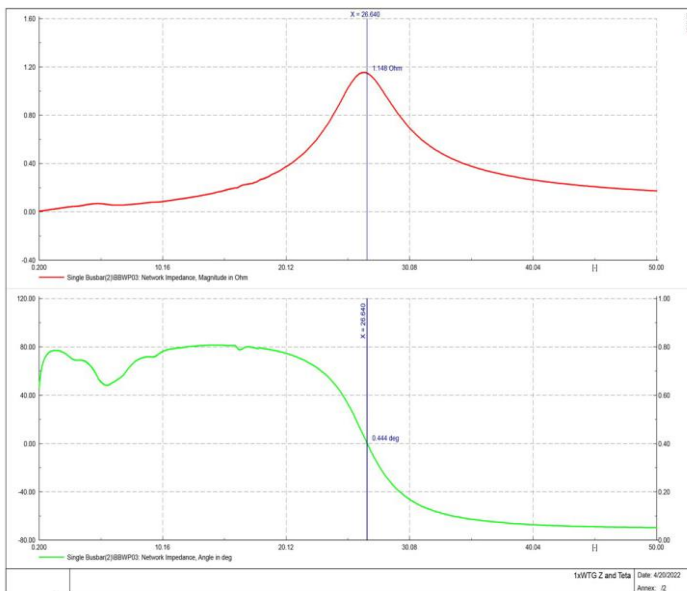
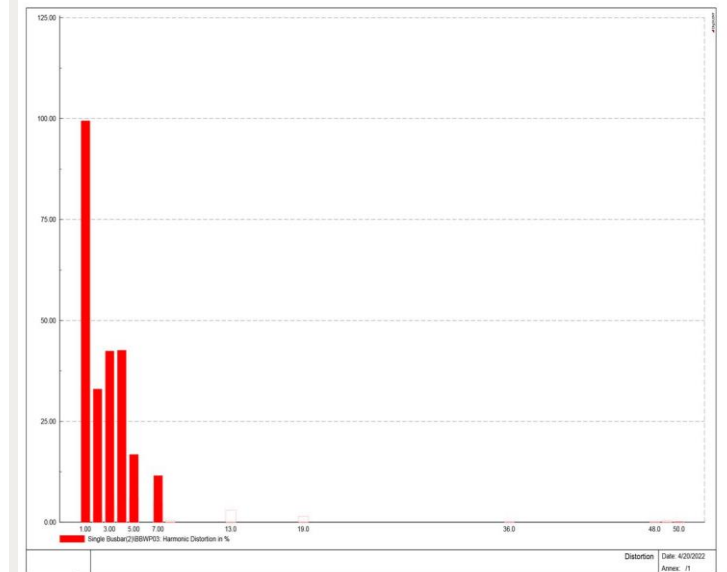
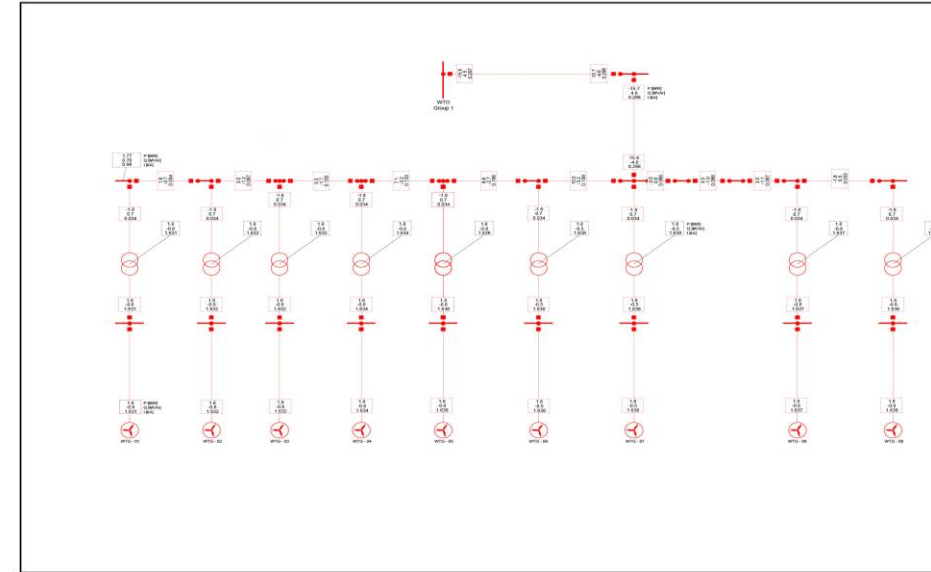
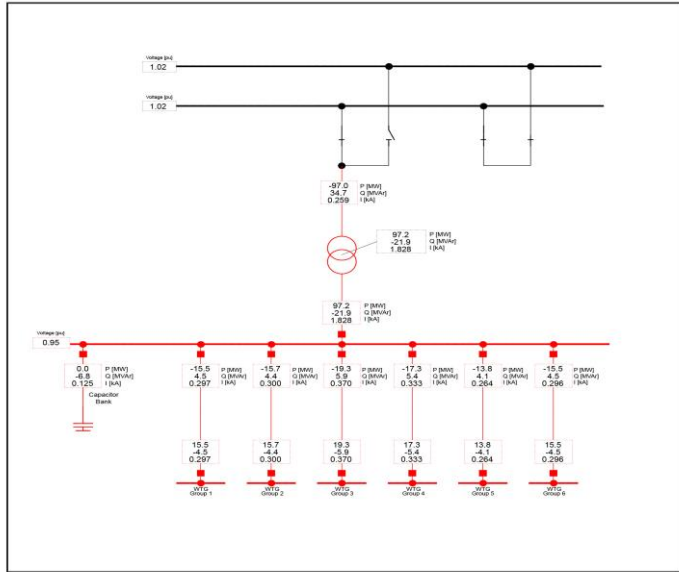
Influence from Harmonic (Subharmonic) on Protection System Performance – Real Disturbance on BIPS



Subharmonics: 6, 20 and 30 Hz (10% 60 Hz)

- Protection IEDs will work with one sliding FT window → beind able to capture the 3 fault cycles, but to perform harmonic content, capturing the subharmonic the sliding window size should be → 60 Hz/5Hz or 12 data cycles;
- If the protection IEDs work with one sliding window with 12 data cycles length → it will be possible to discriminate the subharmonic → however, its processing will include time delay.
- The subharmonics can cause instability on the phasor domain processing (DC shift), thus, causing instability/oscillation in frequency/angle estimation by IEDs (under/overreaching, for example by 21/21N elements)

Influence from Harmonic (Subharmonic) on Protection System Performance – Simulated System EMT Software



The main points can be highlighted, in general, as:

- Necessary to have correct representation of voltage harmonic sources of WTG, in the EMT simulation tools;
- Necessary to have adequate modeling for the WTG controls, including Phase-Locked Loop (PLL) which will influence the frequency/angle behavior;
- Adequate representation of the electrical network, in order to verify the points of parallel resonance → overvoltage!

Conclusions and Main Recommendations:

- During the fault, the transient response of the inverter can compromise the behavior of the fundamental components and add other frequency components in the output signals;
- The estimation algorithms used in commercially available relays are sensitive to interharmonics and subharmonics, depending on the quantities → instability/oscillation of the phasors can occur;
- Due to phase estimation errors, the Zone 1 relay distance element at PCC may overreach for internal faults close to the remote terminal. Further analysis is needed to avoid maloperation of Zone 1 for external faults near the remote terminal. Changes to the Zone 1 configuration guidelines may be required;
- Line differential protection schemes tend to work correctly for most cases, regardless of phase estimation errors;
- Models suitable for EMT tools must be taken into account for the simulations;
- The manufacturer's recommendations of IEDs have been adopted as best practices, however, it is understood that the problem is not yet solved and needs further research and proper investigation;
- The use of time domain protections with phasor domain protections should also be evaluated;
- Finally, it is recommended to evaluate the local protection but also the remote distance and directional protections (up to adjacent busbars), for the coordination schemes.