

## Study Committee B2

Overhead Lines

11074\_2022

### Probabilistic safety concept in OHL construction

Stefan STEEVENS<sup>1</sup>, Erick ULLOA JIMENEZ<sup>2</sup>, Niklas WINKELMANN<sup>3</sup>, Matthias MIX<sup>2</sup>

Amprion GmbH<sup>1</sup>, Kina Ingenieurgesellschaft mbH<sup>2</sup>

#### Motivation

- The decision to push ahead with the energy transition poses major challenges for transmission grid
- Efficient and safety transmission grid is required
- Construction of DC links, expansion and refurbishment of existing AC grid
- Probabilistic safety concept offers an interesting technical approach for challenge of rehabilitation of existing networks



Figure I: Increasing use of renewable energy

#### Method/ Approach

- With normative basis from DIN EN 1990 all pylon locations can be assigned to different reliability levels by evaluating possible damage consequences
- With the stochastic models of probabilistic, actions and resistances can be described very accurately
- By comparing the determined and required reliability levels an efficient stability verification of lattice pylons can be carried out
- Risk-considered refurbishment of the energy transmission grid

#### Objects of investigation

- As part of a case study we calculated the reliability indices for a pylon based on the load case pressure failure
- Two pressure diagonals in the wall perpendicular to the line of a supporting pylon are considered

#### Experimental setup & test results

- The forces are triggered exclusively by the gust velocity pressure
- The system failure probability is about 1.5 times higher than the highest component failure probability
- A system reliability index of 3.6 was determined, resulting in a reliability level 2 for the pylon.

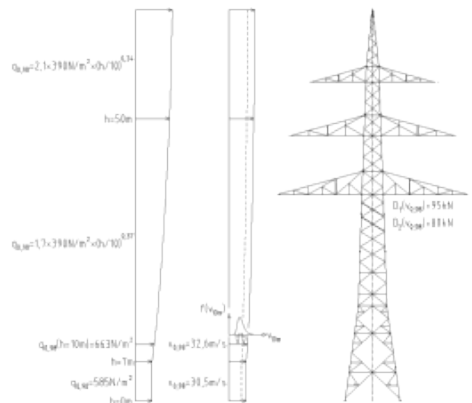


Figure II: Pressure diagonals in the wall perpendicular to a support pylon

#### Discussion

- If the pylon was located closed to a railway, it would have been assigned reliability level 3
- With reliability index of 3.6 this pylon would be clearly above the requirements and the proof would thus be provided

#### Conclusion

- Actions and resistances can be described very accurately
- Efficient stability verification of lattice pylons
- Risk-considered refurbishment of the energy transmission grid and effective use of resources
- Great technical potential to ensure electrical supply security for the energy transition and in the long term with a stable power grid

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#### Method/ Approach

##### Classification of the safety concepts

- Various safety concepts have been used in the past or are used today

Safety concept	Level	Value for the reliability	Design requirement
Deterministic (empiric)	0	Global safety factor n	existing $s \leq$ allowable $s =$ critical $s / n$
Semi-probabilistic	I	Partial safety factors $B_{w, B_s}$	existing $s (B_w \times S) \leq$ critical $s / B_s$
Probabilistic (approximation)	II	Reliability index b	existing $b \geq$ required b
Probabilistic (exact)	III	Probability of failure $P_f$	existing $P_f \leq$ allowable $P_f$

Table I: Classification of the safety concepts

- In case of recalculations of existing structures a partial safety factor is set too high for simplification reasons, may lead to a replacement of the supposedly undersized cross-sections

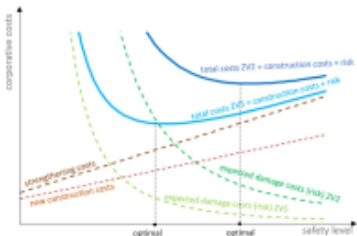


Figure III: Optimal safety level

- Replacement with higher dimensioned components is more expensive than use of same components in new construction (construction site, anchoring work, decommissioning)

#### Reliability level for towers

Required reliability indices of the pylon system (according to table 7 VDE-AR-N4210-4:2014-08)				
Reliability level	required $\beta_{\text{extreme}}$	generated $\beta_{\text{extreme}}$	Site-dependent hazard	examples
1	4.3	$8.5 \cdot 10^{-6}$	very high	stadiums
2	3.8	$7.2 \cdot 10^{-5}$	High (reference)	motorways
3	3.3	$4.8 \cdot 10^{-4}$	Medium	Railway station building
4	2.9	$1.8 \cdot 10^{-3}$		Parking spaces
5	2.6	$4.7 \cdot 10^{-2}$	Very low	Forest area

Table II: Safety levels and target safety indices<sup>sw</sup>

- Target reliability index  $\beta=3.8$  obtained by recalculation of pylons designed according to EN50341-3-4 (1-year extreme)
- Reliability level 1 for higher site-dependent hazards ( $\rightarrow$  3-5 times smaller damage consequences)

#### Verification procedure

- Verification is carried out by comparing the existing reliability index with the required index
- Each component of a steel lattice pylon can lose its function due to several failure mechanisms (components)
- The entire system fails, if a single component fails

#### Limit state functions

- Difference function between capacity (resistance of a component) and the stress consuming (stress or internal force) caused by external actions

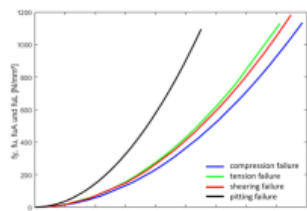


Figure IV: Limit state functions in the original space for four failure modes

#### Stochastic models

- For probabilistic calculation stochastic models must be set up
- For the stochastic modelling of the gust wind speeds  $v$ , an extreme value distribution type III with variation coefficient and a positive curvature parameter is assumed (VDE-AR-N 4210-4)

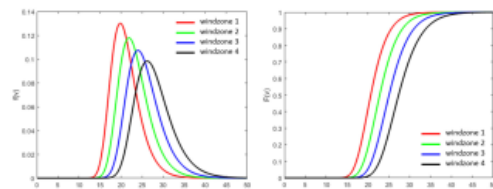


Figure V: Distribution density and cumulative distribution functions Extreme value type III of the gust wind speeds (10m above ground level)

- The stressability of all failure modes is described by means of a lognormal distribution (VDE-AR-N4210-4, 7.3.6)
- With distribution parameters mean value  $m$  and standard deviation  $\sigma$  the distribution density and cumulative distribution functions can be created

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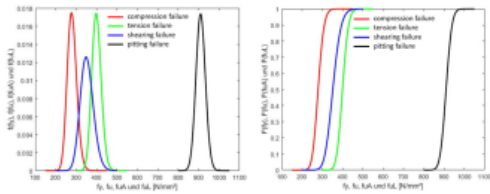


Figure VI: Distribution density and cumulative distribution functions of the lognormal yield strength (S235) and distributed strength

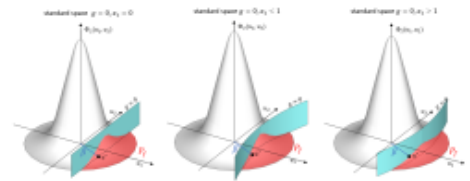


Figure X: Representation of the limit state function in standard space

#### Standardisation

- Limit states are then transformed into the standard space and the design point determined, which is located on the limit state with the smallest distance to the origin

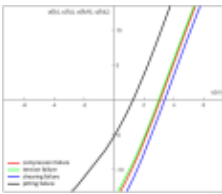


Figure VII: Limit state functions in standard space

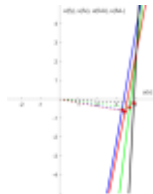


Figure VIII: Reliability index

#### Reliability index of a system

- Sensitivities are calculated from the design point and the reliability index, the correlation matrix can be created
- Once all component failure probabilities are known, the system failure probability must still be calculated
- A system failure already exists when the first component fails
- The system failure probability of a series system is always higher than the highest component failure probability

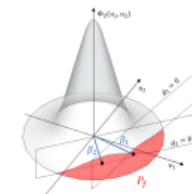


Figure XI: Failure space for two components

- Length of this distance is the reliability index  $\beta$  of the component

- The reliability index is calculated from the failure probability of the overall system which is compared with the required reliability level of the site

#### Conclusion

- Actions and resistances can be described very accurately
- Efficient stability verification of lattice pylons
- Risk-considered refurbishment of the energy transmission grid and effective use of resources
- Possibilities through more precise considerations on the side of impacts (weather parameters)
- Safety concept for lattice pylons can be applied to other areas of the energy grid
- Great technical potential to ensure electrical supply security for the energy transition and in the long term with a stable power grid

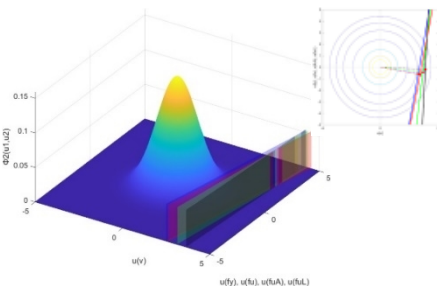


Figure IX: Bivariate standard normal distribution and limit functions in standard space

- The FORM solution is an approximation that can be improved by calculating the curvatures of the limit state in addition to the coordinates of the design point
- The more exact SORM solutions can be calculated