



Study Committee B4 DC SYSTEMS & POWER ELECTRONICS

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A transparent process to ensure appropriate and compliant grid-forming behavior for HVDC systems and FACTS – A TSO perspective

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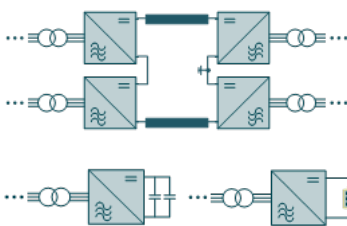
1. Motivation

- Grid-Forming converters are foreseen to play a major role in the future European power system
- German TSOs see a compelling necessity to equip all new converters that are directly connected to the transmission system (e.g. HVDC and STATCOM) with grid-forming controls
- Paper aims to describe the lessons learned from the specification phase of different assets with grid-forming requirements
- Focus lays on the verification procedure and conformity testing methods of grid-forming behavior

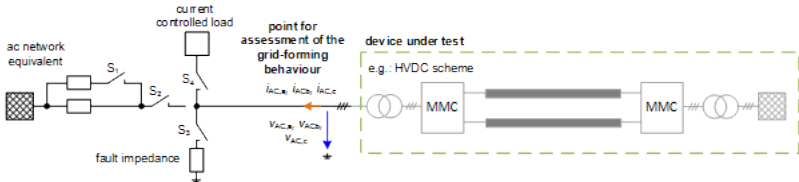
2. Future Assets with Grid-Forming Capability

- Three different groups of PEIDs¹ with grid-forming capability are planned to be integrated into the grid: *embedded HVDC*, *STATCOM-GFC* and *Grid-Booster*
- Grid-forming behavior will be required for all of the aforementioned assets
- However, requirements on individual grid-forming design aspects differ due to different physical constraints (e.g. available energy reserves)

Embedded HVDC, STATCOM-GFC and Grid-Booster



Test network for assessment of the grid-forming behavior of a device under test

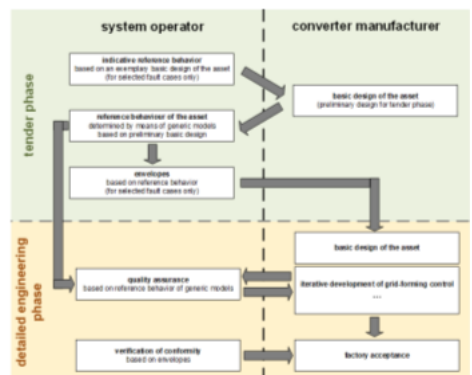


¹ Power electronic interfaced devices (PEIDs)

3. German FNN Guideline: Fundamentals & Application

- German FNN guideline provides guidance terms of specification and conformity testing methods for grid-forming assets
- Grid-forming behavior of the asset shall be verified by means of EMT-simulations
- Benchmark system comprising test network and typical test cases (e.g. phase angle or voltage magnitude steps, frequency changes, change in network impedance, islanding with current controlled load etc.)
- Basic idea: TSO specifies a reference behavior for each test scenario by means of simplified models and creates “envelope” curves

Sequence diagram of an exemplary application of the FNN guideline



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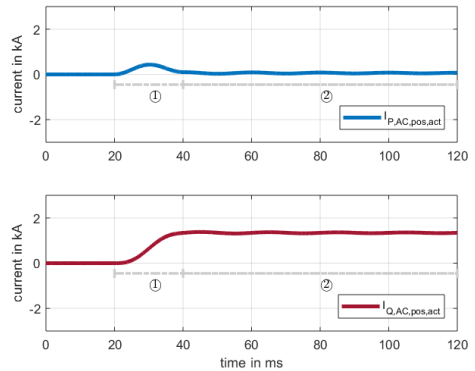
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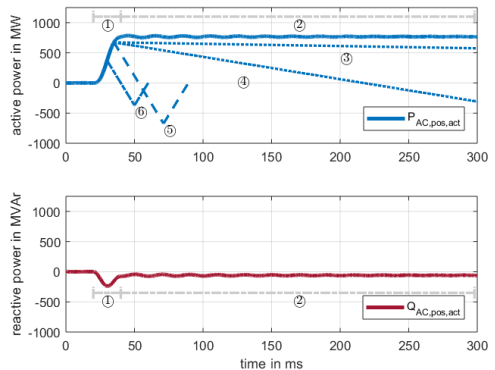
4. Dynamic Performance of GFCs: Exemplary System Behavior

- The system behavior during a **3-phase-to-ground fault** can be divided into different time periods:
 - Instantaneous response of DUT:
 - Immediate increase of reactive current contribution at the PCC
 - Instantaneous characteristic of the DUT
 - Fast current limitation schemes needed to protect power electronic components
 - Duration: up to two grid cycles
 - Steady state fault current contribution:
 - Quasi-stationary operating point is reached within approx. one grid cycle
 - DUT provides a constant but parameterizable reactive current
- The system behavior during a **phase angle step (-10°)** can be explained as follows:
 - Instantaneous response of DUT:
 - Immediate increase of active power at the PCC
 - Instantaneous characteristic of the DUT
 - Fast current limitation schemes needed to protect power electronic components
 - Required for all three groups of assets mentioned in Section 2
 - Transition behavior:
 - Return to a steady state power set point
 - ③-⑥ additional design-related degree of freedom (asset specific, depending on available energy reserves)
 - ③ slow decaying response might be achieved with additional battery storages (e.g. grid-booster)
 - ④ medium decaying response might be achieved for assets equipped with additional supercapacitors (e.g. STATCOM-GFC)
 - ⑤-⑥ fast return of the active power component required due to very limited energy reserves (e.g. embedded HVDC)

Exemplary reference behavior of the DUT during a three-phase-to-ground fault at $t = 20$ ms (residual voltage 80 %)



Exemplary reference behavior of the DUT during a phase angle step in network voltage at $t = 20$ ms (-10°)



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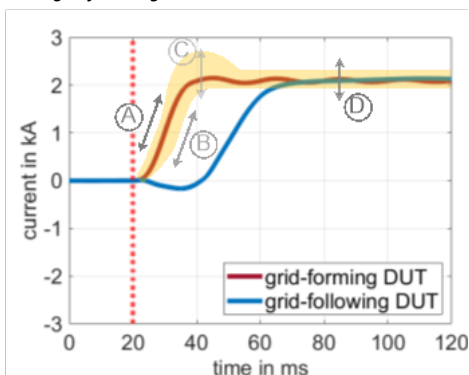
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5. Exemplary Determination of Envelopes

- Basic idea: keep the system behavior of the asset close to the specified reference behavior, but allowing room for manufacturer dependent control implementations or basic design differences
- Exemplary procedure to determine an appropriate envelope curve is described for a symmetrical fault:
 - Relevant quantity: reactive current component of the positive sequence $I_{QAC, pos, act}$
- A) Upper boundary of envelope curve:
 - Instantaneous reaction of DUT
 - Rate-of-rise depends on quantity determination (e.g. filtering of IEC calculation method)
 - Rate-of-rise is limited by impedances between converter and PCC (e.g. transformer leakage reactance)
- B) Lower boundary of envelope curve:
 - Instantaneous reaction of DUT
 - Relevant to distinguish between grid-forming and grid-following DUTs
 - Signal acquisition and filtering stages typically lead to delayed system responses in grid-following converters compared to grid-forming DUTs
- C) Overshoot:
 - Overshoot permissible due to grid-supporting effect
- D) Quasi-stationary accuracy:
 - Steady state fault current contribution
 - Similar behavior between grid-forming and grid-following converters possible
 - Reactive current component of the DUT is proportional to the voltage deviation at PCC and quasi-stationary impedances or proportional factors (e.g. definition of k -factor in grid-following HVDC converters)

Exemplary determination of an envelope curve for $I_{QAC, pos, act}$ (yellow area) – system behavior during a three-phase-to-ground fault for a grid-forming DUT and a grid-following DUT



6. Conclusion

- In line with the system needs related to power electronic-dominated grids, a proper and straightforward specification process of grid-forming behavior is required in order to mitigate the risks for all involved parties in a project
- Paper provides insights into the specification process of grid-forming behavior from the point of view of a German TSO
- Obtained results are relevant for other TSOs, converter manufacturers as well as academia and provide a structured process to benchmark the functional requirements regarding control implementations in case of assets with grid-forming controls