





Paraíba (UFPB)

Study Committee B5 Protection and Automation

Paper ID 10147

FROM HERTZ TO MEGAHERTZ: LESSONS LEARNED ABOUT THE IMPACT OF INVERTER-BASED WIND TURBINE GENERATORS ON THE PROTECTION OF INTERCONNECTING LINES

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Motivation

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- Massive integration of Inverter-Based Resources (IBRs) have resulted in great changes in electrical power grids
- Wind IBRs (WIBRs) already accounts for about 12.5% (2022) of the total Brazilian generation capacity
- Traditional protection schemes have been challenged!
 Various solutions have been developed
 - Several researches → LESSONS LEARNED TO SHARE!

Evaluated Topologies

- This work is focused on two types of WIBRs
 - Doubly-Fed Induction Generator (DFIG/Type III)



Two connection paths:

- 1) Stator to the grid;
- 2) Rotor windings via an AC-DC-AC converter

Full Converter Generators (FC/Type IV)



✓ Only one path → Completely decoupled (≈ PV plants)

1) Connected via an AC-DC-AC converter

Atypical Fault Contributions of IBRs

- Conventional synchronous generators have high inertia
 - - Relevant fault current contributions
 - Well-defined voltage angles
- IBRs are governed by converters
 - Control strategies define how DFIG and FC units ride through faults → Atypical fault contributions
- · Fault response often verified in systems with WIBRs
 - DFIG → Fault currents up to 2 pu
 - FC \rightarrow Often limited to 1.2 pu
 - Crowbar operation and control strategies can result in relevant frequency deviations
 - Low fault current contributions
 - Voltage angles difficult to predict
 - Uncertainties on the presence of certain sequence components, etc

Grid Codes

- Grid codes have been proposed to avoid multiple control strategies in the same power system
- A variety of grid codes can be found and they are under development in several countries
- In this work, two grid codes are evaluated:
 - An European Grid Code (EGC) (see paper references)
 Reactive current emulation
 - An American Grid Code (AGC) (see paper references)
 - No reactive current emulation

Topology of Typical WIBRs Interconnection to the Power Transmission Grid



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Lesson 1: "Not everything is 'control'. The interconnection circuit topology matters!"

- It is common to hear: "converter controls cause the problem of WIBR' fault response"
 - Control strategies limit positive and negative current sequence contributions
 - Grounded neutrals lead the fault to be dominated by zero sequence quantities in grounded faults
 - Being dominated by zero sequence currents usually minimizes protection issues
 → It is a system contribution rather than a WIBR contribution



Lesson 2: "Atypical WIBR fault contributions are not limited to fault current levels"

- Study on fault current contributions based on EMTP simulations and real record studies
- Low fault current contributions consist in only one of the possible impacts -> Synchronous generator >> DFIG > FC
- Angles of electrical quantities may vary during the fault period \rightarrow Quite challenging for protection functions!



- Fault-induced high frequency components follow the classical theory of electromagnetic transients
- DC decaying component varies with the fault inception angle (here, sinusoidal ref.) → Synchronous generator > DFIG > FC



Lesson 3: "Pay attention to digital phasor estimation filters"

- Phase-locked-loop (PLL) schemes are used to estimate system voltage frequency and amplitude → It drives the inverters!
- Errors in estimated frequencies can occur
- Spurious frequency components can take place
- Synchronous Reference Frame (SRF-PLL) [19] and Dual Second Order Generalized Integrator (DSOGI-PLL) are evaluated
- Full-cycle (F1, F2) and half-cycle (H1, H2) phasor estimation filters are assessed







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Lesson 4: "Blind zones on the interconnecting line may exist if communication is lost"

- Differential protection and pilot protection schemes have shown to be promising → The need for a communication channel is a drawback → Is the non-unit protection reliable?
- PS Simul EMTP massive simulations and playback tests using the CE-7012 test box + real microprocessed relays from 4 different manufacturers (firmware versions from 2018) → Evaluation of instantaneous operation percentage of: 87, 21 and POTT+Weak Infeed schemes



Lesson 5: "EMTP models must include stray capaci "

- Results on the busbar stray capacitances are presented in this work. Transformer stray capacitances must be also considered
- Evaluation of a traveling wave-based differential element, varying the busbar stray capacitance, for different fault resistance R_F → Conclusions are different!
- Realistic modeling is mandatory to avoid misinterpretation on the performance of transient-based protection functions



Lesson 6: "For each system, a particular study. Uncertainties are inevitable!"

 Sources of uncertainty: Diversity of grid codes, control strategies, interconnection topologies, IBR features, use of BESS, increasing IBR insertion at remote terminals, crowbar operation, protection particularities, and so on



Lesson 7: "Directional elements will not always fail. It depends on the fault location"

- Many people thinks that directional elements will always fail in systems with IBRs, but it depends on the fault location
- Negative sequence element: FWD: Z2 < thr+ and REV: Z2 > thr+



Conclusion

- Innovative solutions have been developed, specially to improve non-unit protection
- Alternative operating characteristics, enhanced phasor estimation solutions, use of voltages rather than currents for phase selection, analysis of fault-induced transients, reduced decision-making time, communication redundancy, and so on
- Uncertainties are inevitable and more challenging scenarios are coming soon
- Reliable open-source EMTP models are of paramount importance for future developments

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