

Study Committee C2

SYSTEM OPERATION AND CONTROL

Paper ID 10427

Low Demand Operation of an Islanded Grid with High Share of Inverter-Based Resources – South Australian Case Study

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Introduction

- § South Australia (SA) has the world leading integration of IBR and Distributed PV (DPV). The increasing level of IBR has accelerated the retirement of SGs.
- § Four large synchronous condensers (SCs) are installed in SA to provide system strength.
- High DPV generation has reduced the minimum demand in SA, leading to voltage rise issues during low demand conditions.
- High DPV generation can increase the size of the MW contingency, for a fault around DPVrich area, causing unintended tripping of DPV.
- The above have complicated voltage and frequency control, under low demand operation of SA island.

Power System Modelling

- The wide-area EMT model of SA grid was used.
- The model includes detailed and where applicable site-specific models of all network elements.
- The model is benchmarked against measured responses during the actual grid events.
- DPV trip was modelled via an equivalent increase in the size of the contingency.

Figure 1 Record low operational demand in SA power network

Frequency Control

50.2

₅₀ 室 49.8 49.6 49.4 49.2 49 48.8

15 16 17

- 150 MW DPV
Disconnectic

225.00

200.00

- Displacement of SGs in SA has reduced the physical inertia and frequency control in SA.
- Four SA SCs provide inertia through their flywheels, but not frequency control.
- § During SA island, three SA BESSs are dispatched to 0 MW to have two-way FFR headroom.
- § During low demand condition, high DPV generation can lead to increased size of contingency for a fault close to the DPV-rich area (unintended PV trip).
- To control the frequency, the maximum size of contingency should be limited.
- § **Simulation Results:** When the size of contingency is below 175 MW, the frequency can be arrested without violating the UFLS threshold. This may require curtailing DPV generation during low demand periods.

19

175 MW DPV

me (s)

 (a)

22 23

200 MW DPV

 (b)

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Frequency Control: Impact of IBR generation level

- The IBR generation level can impact the maximum allowable size of contingency.
- § Simulation results show that in a case with higher IBR generation, a smaller contingency size should be allowed to get the same frequency nadir.
- § **Reason:** the temporary energy deficit caused by FRT behaviour of IBRs is larger at higher IBR levels.

Frequency Control: Impact of Extra SGs

- The location of SG in the network has an **impact:**
	- \triangleright If the SG is at distribution level, there would be less impact on the contingency size.
	- Ø **Reason:** A fault at the terminal of the SG does not cause IBR go through FRT mode.
	- \triangleright A higher contingency size can be allowed, when a distribution SG is brought online.

Figure 3 (a) Total IBR generation (b) Frequency (Hz)

Frequency Control: Impact of Extra SGs

- § Additional SGs increase the inertia and primary frequency response (PFR). **However**:
	- v **In SA, most SGs are close to DPV-rich metro area:**
		- An extra SG could increase the contingency size.
		- Ø A fault at the terminal of a SG (close to metro) can trip the SG and some DPV too.
		- With an extra SG, more pre-emptive DPV curtailment may be required.

Voltage Control

- Under low demand conditions of SA island, the generation from transmission-connected generators needs to be reduced to balance the low demand.
- Low demand, caused by high DPV generation, cause very low flows through the lines.
- The capacitive charging of lightly loaded lines can cause high voltages across the network.
- § Four SCs and four SVCs in SA may not be sufficient to lower the high voltages under too low demand levels.
- Extra voltage control measures are needed.

Table 1: Maximum size of contingency with different SG combinations

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Measures for Lowering the Voltages:

- All cap-banks should be switched out and all reactors should be switched in.
- § Four SVCs and four SCs should absorb reactive power as per their capability. A 30% pre-fault Q headroom was considered for SVCs and SCs.
- § Transmission-connected SFs should absorb reactive power within their capability. SFs are likely to be available during (sunny) high DPV generation hours.
- All online WFs together absorb a total of 100 MVAr. If WFs are not available (low wind, etc.), switching out a line in the North area can lower the voltages.
- As the last resort, extra SGs can be dispatched for voltage control support. The number of SGs needed depends on the operational demand level.

Need for Additional SGs:

- § **Worst contingency:** trip of an SVCs absorbing large reactive power pre-fault
- Two cases were simulated, with and without an extra SG online. SA demand is 300 MW and all voltage control measures are already in place.
- Without a SG, post-fault voltages go too high. Also, SCs and SVCs violate 30% pre-contingent Q headroom.
- \div Demand level below which extra SG is needed:
- o **Scenario A:** High availability of reactive power
- o **Scenario B:** Low availability of reactive power

Figure 5 Need for extra SGs at different demand levels

Figure 4 Impact of extra SG on voltage control

Conclusions

- Two challenges for operating SA island under low demand condition: frequency and voltage control
- Under low-demand high-DPV generation, the size of contingency should be limited through pre-emptive DPV curtailment or reducing the generation by SGs.
- Extra SG close to DPV-rich area may increase the size of contingency and necessitates more DPV curtailment.
- At high IBR levels, smaller contingencies can be allowed, due to energy deficit caused by FRT behaviour of IBRs.
- At low demand levels, additional SG(s) may be required for bringing the voltages down.
- The lower the demand level the more SGs will be needed for voltage control.