

## Study Committee D1

Materials and Emerging Test Techniques

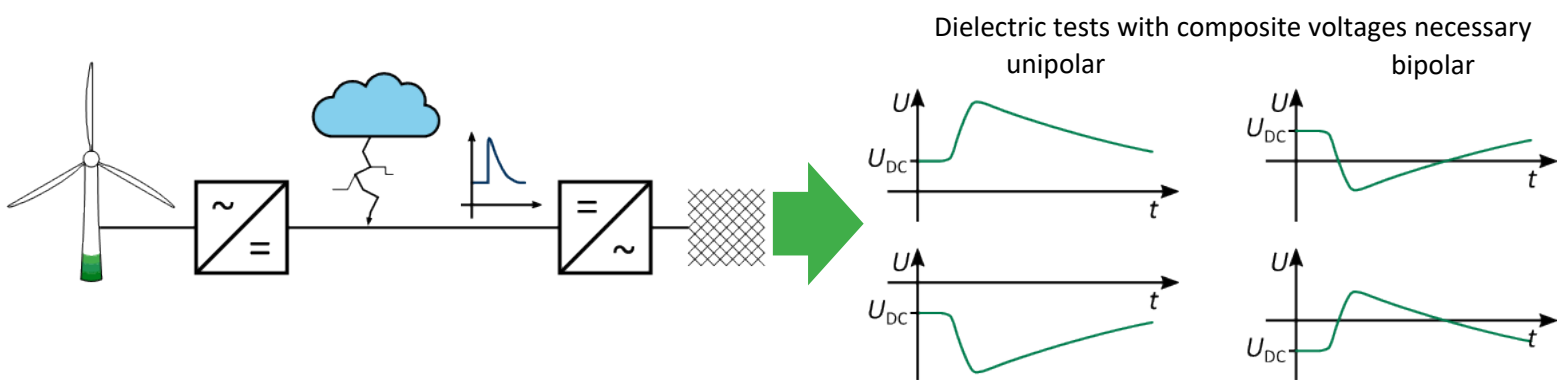
Paper D1-PS1-11116

### Impact of Different Blocking Elements on the DC-Impulse Composite Waveform

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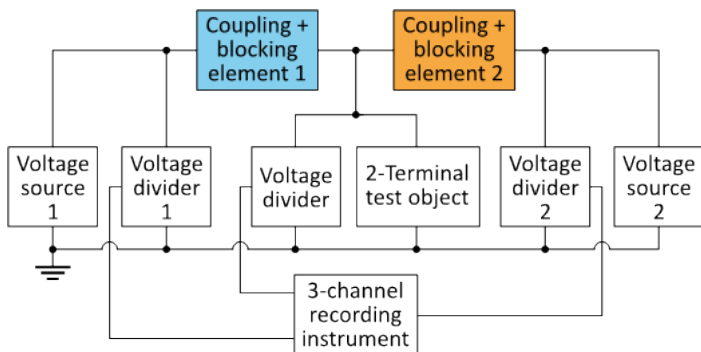
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#### Motivation



#### State of the Art

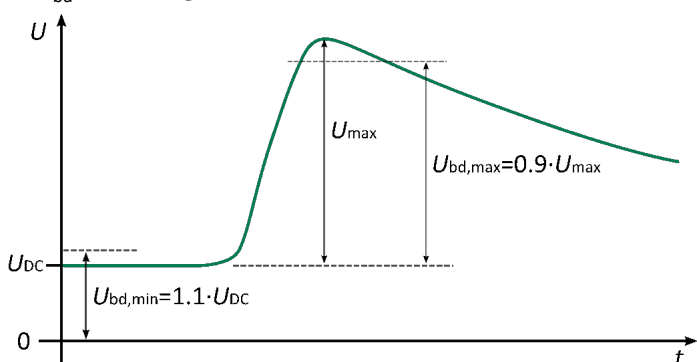
- IEC 60060-1 defines a general test circuit to superimpose two voltages to one test object (DUT)
- Coupling and blocking elements
  - protect the respective voltage source against the voltage of the other voltage source
  - must couple both voltages to the DUT and should not influence the composite voltage



- Possible coupling and blocking elements to superimpose DC and impulse voltages:

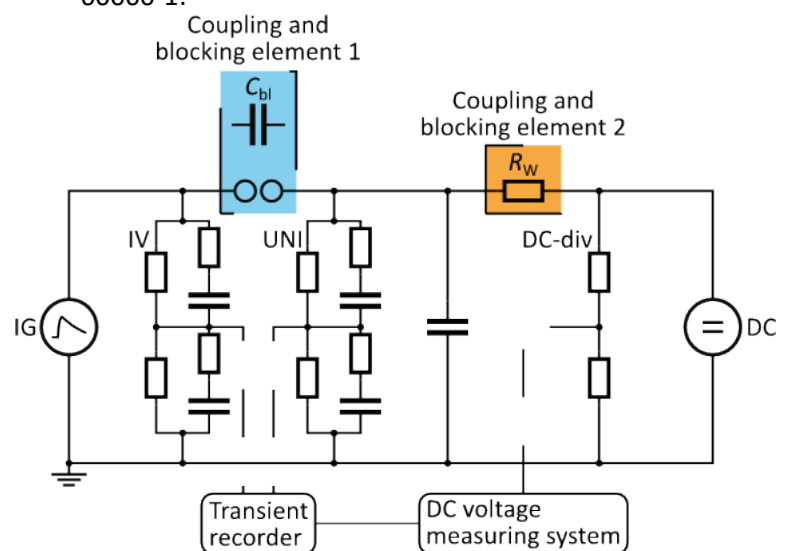
Voltage	Coupling and Blocking Elements
DC	...
Impulse	...

- Adjustment of the spherical spark gap ignition voltage  $U_{bd}$  according to IEC 60052



#### Experimental Techniques

- Implementation of the test circuit according to IEC 60060-1:



- $C_{bl}$  Blocking capacitor
- $C_{DUT}$  Device under test
- DC DC voltage source
- DC-div DC voltage divider
- IV Impulse voltage divider
- IG Impulse voltage generator
- UNI Universal voltage divider
- $R_W$  Protection resistor
- SG Spherical spark gap

- Combinations of the coupling and blocking elements investigated:

Coupling and blocking element 1	Coupling and blocking element 2	
	$R_{W1} = 6 \text{ M}\Omega$	$R_{W1} = 1 \text{ M}\Omega$
$C_{bl1} = 17.5 \text{ nF}$	X	X
$C_{bl2} = 11.6 \text{ nF}$	X	
SG: $d_1 = 25 \text{ cm}$	X	X
SG: $d_2 = 10 \text{ cm}$	X	

- Tests with and without short-circuited coupling and blocking element and with and without DC voltage
- Evaluation of the parameters according to IEC 60060-1 from 10 test executions :  
Test voltage  $U_p$ , peak time  $T_1$  and time to half-value  $T_2$

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## Impact of Different Blocking Elements on the DC-Impulse Composite Waveform

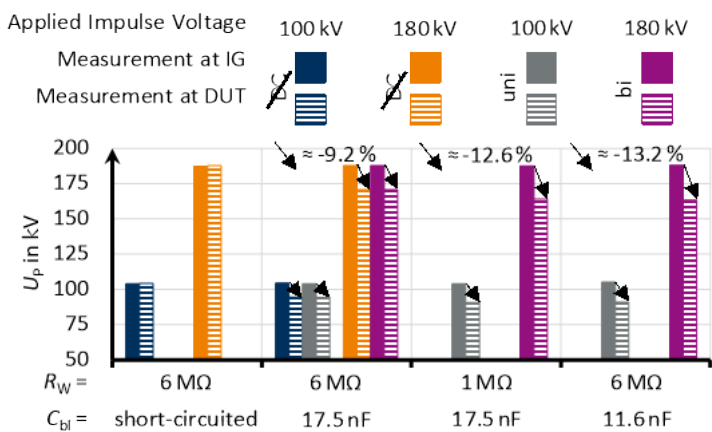
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### Experimental Results

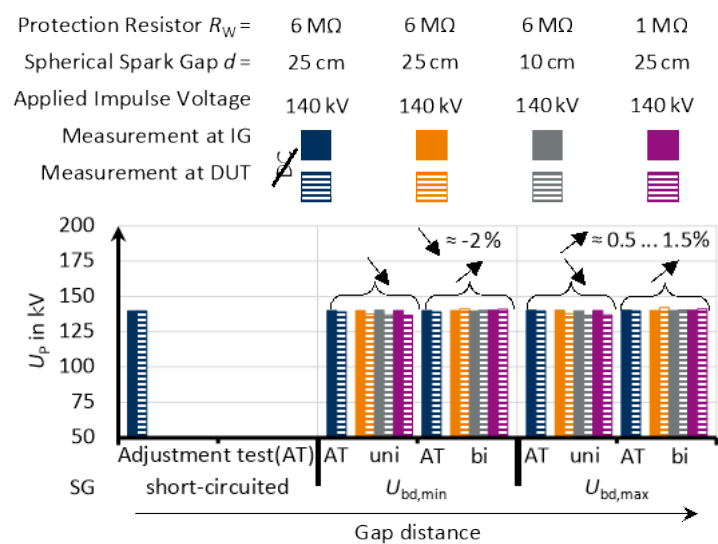
#### Blocking Capacitor

#### Spherical Spark Gap

##### Peak Voltage $U_p$



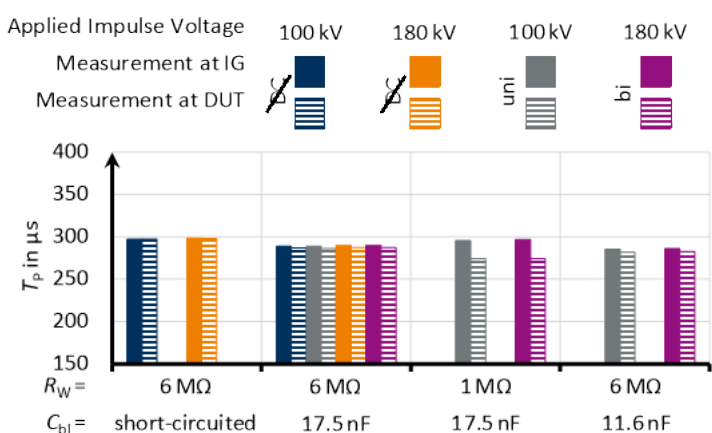
- Utilisation of a blocking capacitor leads to a reduction of the peak value  $U_p$  at the DUT
- Applied DC voltage has no influence on the peak value
- Small blocking resistor  $R_W$  does not fulfil its decoupling task  $\Rightarrow$  further reduction of the peak value  $U_p$  at the DUT



- Deviations of  $U_p$  between IG and DUT are significantly smaller when using a SG instead of a blocking capacitor

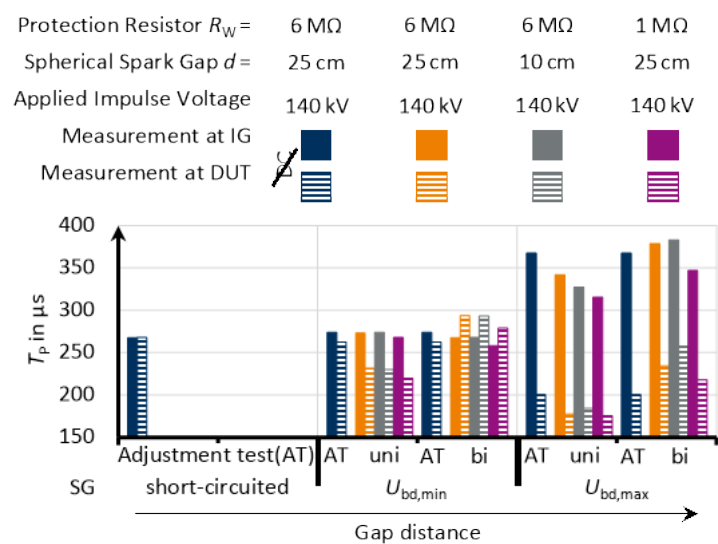
##### Peak Time $T_p$

- Shorter peak Times  $T_p$  can be measured at the IG and DUT, when a blocking capacitor is utilized (not short-circuited)  $\Rightarrow$  Smaller load capacitance because of the series connection of the blocking and DUT capacitance



- A smaller capacitance of the blocking capacitor leads to shorter peak times
- Applied DC voltage has no influence
- The small blocking resistor  $R_W$  does not fulfil its decoupling task  $\Rightarrow$  further reduction of the peak time  $T_p$  at the DUT

- Without applied DC voltage: Shorter peak times at the IG and larger at the DUT with increasing ignition voltage of the spherical spark gap



- Unipolar applied DC voltage: Further reduction of the peak times at the DUT
  - Bipolar applied DC voltage: Increase of the peak time at the DUT
- $\Rightarrow$  Reason is the different voltage behaviour at the DUT for bipolar and unipolar superposition
- $\Rightarrow$  Unipolar: After ignition of the SG large steep voltage rise at the DUT
  - $\Rightarrow$  Bipolar: Discharge from DC-voltage

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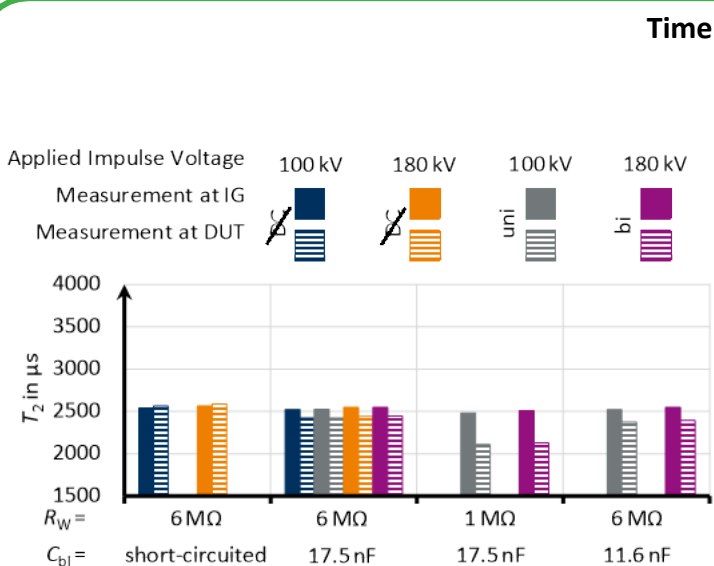
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### Impact of Different Blocking Elements on the DC-Impulse Composite Waveform

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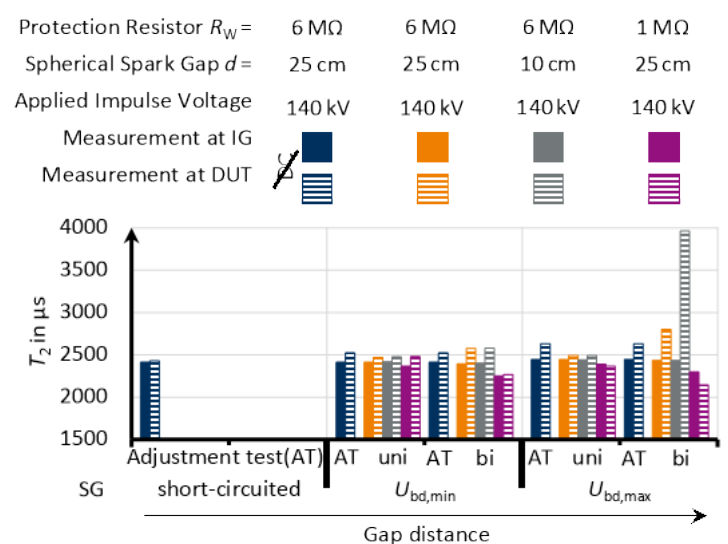
#### Experimental Results (continued)

##### Blocking Capacitor



- The smaller the capacitance of the blocking capacitor, the shorter the time to half-value  $T_2$  at the impulse voltage generator and the DUT
- With connected blocking capacitor the time to half-value  $T_2$  at the DUT is shorter than at the IG
- Applied DC voltage has no influence
- Small blocking resistor  $R_W$  does not fulfil its decoupling task  $\Rightarrow$  further reduction of the time to half-value  $T_2$  at the DUT

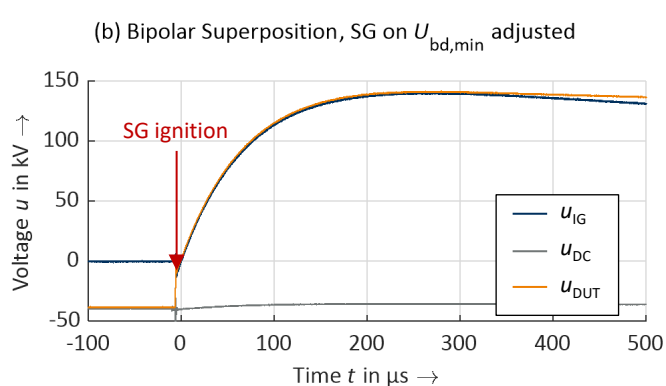
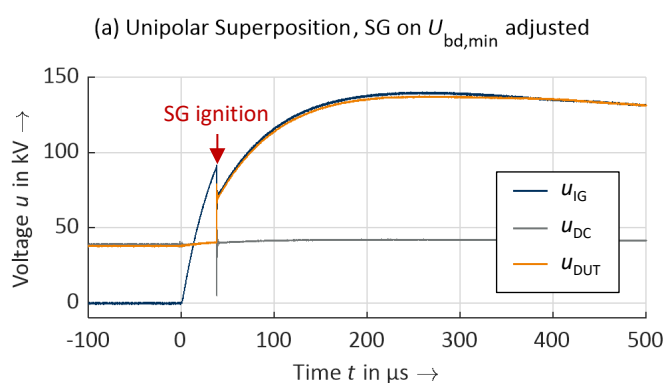
##### Spherical Spark Gap



- Time-to-half-value  $T_2$  remains almost constant at the IG for all investigated sphere diameters, gap distances and protection resistors ( $T_2 = 2424 \pm 33 \mu\text{s}$ )
- Compared to the adjustment tests the time-to-half-value increases for unipolar and decreases for bipolar superposition of DC and impulse voltage
- Sphere diameter has no influence on the time to half-value  $T_2$  (outlier for bipolar superposition because of extinguishing of the SG)

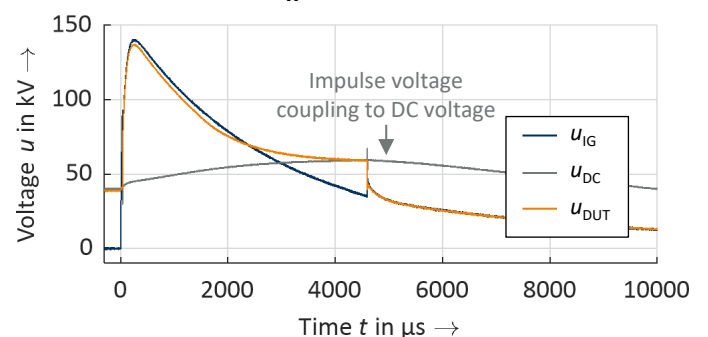
#### Selected composite voltage waveforms

##### Uni- and bipolar superposition with spherical spark gap



- Differences in the time parameters between uni- and bipolar superposition because of the different ignition behaviour of the spherical spark gap

##### Small blocking resistor $R_W = 1 \text{ M}\Omega$ and spherical spark gap



- Coupling of the impulse voltage to the DC voltage due to too low blocking resistance

#### Conclusion

- IEC60060-1 time parameter adjustment should be carried out with utilized coupling and blocking element
- Blocking resistor has to be chosen large enough to not couple the impulse voltage to the DC voltage
- Steep rise of voltage is not covered by the evaluation process of the time parameters according to the standard IEC 60060-1